# TIBIOFEMORAL SURFACE MODELING FOR JOINT MECHANICS ANALYSIS 

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## INTRODUCTION

Small changes in knee joint mechanics are hypothesized to be a contributing factor in the initiation and progression of osteoarthritis. Our lab will analyze parameters of joint contact mechanics based on the relative position and separation of articulating surfaces (e.g., proximity distance).

This project aimed to optimize an existing Thin Plate Spline (TPS) mathematical surface modeling routine [1] for human bone surfaces. These modifications were necessary to accommodate differences in surface digitization methods, scan resolution, desired surface model grid resolution, and to model the highly curved femoral surface. There were three main research objectives: (1) determine the number of sample points needed to ensure a continuous grid without holes, (2) determine a method to model curvatures greater than $75^{\circ}$, and (3) determine the degree of surface smoothing.

## METHODS

To answer the first question, the number of surface points (SP) and grid cutting distance (CD) were systematically increased from $5000-9000$ and $1.5 \mathrm{~mm}-2.0 \mathrm{~mm}$, respectively. Fast computation times and a continuous spline grid (i.e., no holes) were the criteria used to determine appropriate SP and CD optimisation parameters.

Two approaches that sectioned the femoral surface into three components were evaluated. Sectioning the femur was done in an effort to circumvent the curvature errors that occurred when modeling the femoral surface (Figure 1a.). Each method rotated the anterior and posterior data tangentially to the xy plane, which reduces spline fitting errors. The most important criterion for selecting the final approach was to keep the seams of the three femoral TPS sections away from the main distal contact area.

Lastly, the amount of tibial smoothing was evaluated over a range of smoothing factors ( $\lambda=0.2-2.2$ ), and the resulting surfaces were compared to completely interpolated and noisy ( 1 mm random noise) surfaces.

## RESULTS

Acceptable grid continuity and computation time ( $\sim 1.7 \mathrm{mins}$ ) were found at 5000 SP and 1.5 mm CD for the tibial surface.

Both 5000 SP with 1.8 mm CD and 7000 SP with 2.0 mm CD gave a continuous femoral spline grid, but resulted in longer computation times. At 9000 SP , the spline grid was always continuous at the cost of greater computation time (10 minutes+ at all CD values), but curvature errors remained.

Sectioning the femoral surface (anterior, posterior and distal) eliminated these curvature errors (Figure 1b). However when tibiofemoral proximity was calculated, significant errors occurred at the two seams of the surfaces.


Figure 1. Sample size of 5000 pts and 2.0 mm CD a) Original TPS fit b) TPS fit with 3 surface sections.

Based on the sensitivity analysis of $\lambda$ values, $\lambda=0.3$ was chosen to test whether this resulted in a sufficient amount of tibial surface smoothing. The chosen smoothing was very close to the interpolated surface, but did not smooth out the added noise sufficiently.

## DISCUSSION AND CONCLUSIONS

Appropriate SP and CD values were determined for tibiofemoral surfaces, and sectioning the femoral surface into three components reduced spline fit artifact at the highly curved anterior and posterior femoral regions. A sectioned femoral surface improved the TPS geometric fit, but errors persisted when tibiofemoral proximity was mapped. The section methods developed here therefore require further refinement for proximity distance mapping. Lastly, more smoothing is likely required for tibial surfaces to be able to smooth out unwanted noise. This work is an important first step towards optimizing tibiofemoral surface modeling used in joint contact mechanics.

## REFERENCES

1. Boyd, SK, et al. J Biomech Eng 121: 525-532, 1999.
